

LECTURE 18

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Let's start with an exercise on computing flux.

Lemma 1. Suppose that a surface S in \mathbb{R}^3 is given implicitly as the set $g(x, y, z) = c$ for some constant c . Then at any point $s \in S$, the gradient $\nabla g(s)$ is a normal vector at s .

Proof. Let $\mathbf{r} : \Omega \rightarrow \mathbb{R}^3$ be a parametrization for the surface near s , where $\Omega \subseteq \mathbb{R}^2$ is some open subset. Then we have

$$\frac{\partial g}{\partial u}(s) = \nabla g(s) \cdot \mathbf{r}_u(s) = 0.$$

The same is true for $\mathbf{r}_v(s)$. Hence $\nabla g(s)$ is orthogonal to both $\mathbf{r}_u(s)$ and $\mathbf{r}_v(s)$, as desired. \square

Example 2. Find the flux of $\mathbf{F} = yz\mathbf{j} + z^2\mathbf{k}$ outward through the surface S cut from the cylinder $y^2 + z^2 = 1, z \geq 0$, by the planes $x = 0$ and $x = 1$.

Solution. View S as the level surface given by the vanishing of $g(x, y, z) = y^2 - z^2 - 1$. By Lemma 1, the unit normal vector field is given (up to a sign) by

$$\mathbf{n} = \frac{\nabla g}{\|\nabla g\|} = \frac{2y\mathbf{j} + 2z\mathbf{k}}{2\sqrt{y^2 + z^2}} = y\mathbf{j} + z\mathbf{k}.$$

By drawing a picture, you can easily see that this is already pointing outward, so we do not need to adjust the sign. Now we use x, y as variables for S . Then

$$d\sigma = \frac{\|\nabla g\|}{|g_z|} dA = \frac{1}{z} dA$$

where $A = dxdy$ is the infinitesimal unit area element on the projection S' of S to the xy -plane. Putting these together, we have

$$\int_S \mathbf{F} \cdot \mathbf{n} d\sigma = \iint_{S'} (yz\mathbf{j} + z^2\mathbf{k}) \cdot (y\mathbf{j} + z\mathbf{k}) \frac{1}{z} dA = \iint_{S'} 1 dA = \text{Area}(S') = 2.$$

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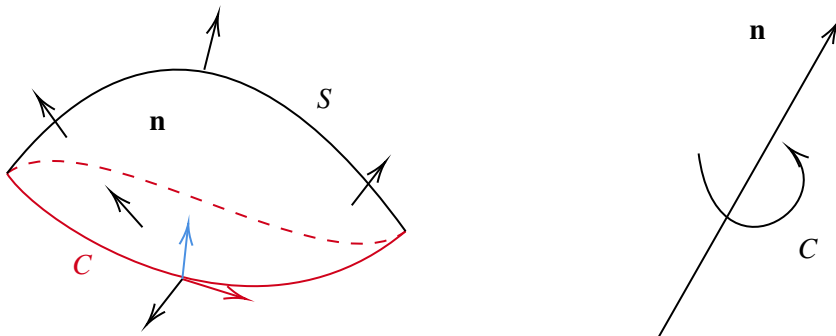
Now let us move on to the Stokes' theorem.

Theorem 3. Let S be a smooth oriented surface having a (piecewise) smooth boundary curve C . Let $\mathbf{F} = M\mathbf{i} + N\mathbf{j} + P\mathbf{k}$ be a vector field whose components have continuous first partial derivatives on an open region containing S . Then

$$\int_C \mathbf{F} \cdot \mathbf{T} ds = \iint_S (\nabla \times \mathbf{F}) \cdot \mathbf{n} d\sigma$$

where \mathbf{T} is unit tangent vector field on C in the counterclockwise orientation with respect to \mathbf{n} .

Recall that on a surface, an orientation is equivalent to a choice of unit normal vector field \mathbf{n} . I find the easiest way to decide the orientation on the curve C is to use the "right hand rule". Namely, you put your thumb in the direction of \mathbf{n} or some point in the interior of S , then the rest of your fingers are pointing in the "counterclockwise orientation" of the C . See the picture below.



If you don't like this, you can also pick a point on the boundary curve C , then the unit tangent vector \mathbf{T} given by the counterclockwise orientation (the red arrow above) and the unit normal vector \mathbf{n} are related by the condition that $\mathbf{n} \times \mathbf{T}$ (the blue arrow above) is pointing inward to the surface.

Example 4. Let us verify the formula using the hemisphere S given by $x^2 + y^2 + z^2 = 9, z \geq 0$ with boundary circle $C: x^2 + y^2 = 9, z = 0$, and the vector field $\mathbf{F} = y\mathbf{i} - x\mathbf{j}$. As usual, we parameterize C using polar coordinates

$$\mathbf{r}(t) = 3\cos t\mathbf{i} + 3\sin t\mathbf{j}, \quad 0 \leq t \leq 2\pi.$$

The tangent vector is

$$\mathbf{T} = \mathbf{r}'(t) = -3\sin t\mathbf{i} + 3\cos t\mathbf{j}.$$

The line integral becomes

$$\int_C \mathbf{F} \cdot \mathbf{T} ds = \int_0^{2\pi} -9 dt = -18\pi.$$

Now let us compute the surface integral. First, compute the curl of \mathbf{F} :

$$\nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ y & -x & 0 \end{vmatrix} = -2\mathbf{k}.$$

We have

$$\iint_S (\nabla \times \mathbf{F}) \cdot \mathbf{n} d\sigma = \iint_{S'} (\nabla \times \mathbf{F}) \cdot \frac{\nabla g}{\|\nabla g\|} \frac{\|\nabla g\|}{|g_z|} dA = \iint_{S'} \frac{(-2\mathbf{k}) \cdot (2x\mathbf{i} + 2y\mathbf{j} + 2z\mathbf{k})}{2z} dA = \iint_{S'} -2 dA = -18\pi.$$

Example 5. Suppose in the above example, we set C to be intersection of the sphere $x^2 + y^2 + z^2 = 9$ and the plane $x + y + z = 0$ instead. The radius of C is still 3 (exercise). Let us compute the circulation of \mathbf{F} along C with counterclockwise orientation using Stokes. In this case, we view C as the boundary of

$$S := \{x^2 + y^2 + z^2 \leq 9\} \cap \{x + y + z = 0\}.$$

It is easy to see that

$$\mathbf{n} = \frac{1}{\sqrt{3}}(\mathbf{i} + \mathbf{j} + \mathbf{k}).$$

on S . We note that $(\nabla \times \mathbf{F}) \cdot \mathbf{n} = -2/\sqrt{3}$ is a constant, so that we conveniently compute

$$\iint_S (\nabla \times \mathbf{F}) \cdot \mathbf{n} d\sigma = \frac{-2}{\sqrt{3}} \iint_S d\sigma = \frac{-2}{\sqrt{3}} \text{Area}(S) = \frac{-18\pi}{\sqrt{3}}.$$

Example 6. Let us find the circulation of the field $\mathbf{F} = (x^2 - y)\mathbf{i} + 4z\mathbf{j} + x^2\mathbf{k}$ around the curve C , where C is the intersection of the plane $z = 2$ and the cone $z = \sqrt{x^2 + y^2}$, oriented counterclockwise.

You can of course do it directly. Let C be parametrized by

$$\mathbf{r}(t) = 2\cos t\mathbf{i} + 2\sin t\mathbf{j} + 2\mathbf{k}, \quad 0 \leq t \leq 2\pi.$$

Then we compute

$$\mathbf{F}(\mathbf{r}(t)) \cdot \mathbf{r}'(t) = -8\cos^2 t \sin t + 4\sin^2 t + 16\cos t.$$

Integrating this from 0 to 2π directly, we get 4π .

Now let us compute this using Stokes, viewing C as the boundary of the cone $z = \sqrt{x^2 + y^2}$ below it. The orientation of the cone should be chosen so that \mathbf{n} points (not straightly) upward.

Use cylindrical coordinates:

$$\mathbf{r}(r, \theta) = r \cos \theta \mathbf{i} + r \sin \theta \mathbf{j} + r \mathbf{k}, \quad 0 \leq r \leq 2, \quad 0 \leq \theta \leq 2\pi.$$

Normal vector:

$$\mathbf{r}_r \times \mathbf{r}_\theta = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \cos \theta & \sin \theta & 1 \\ -r \sin \theta & r \cos \theta & 0 \end{vmatrix} = -r \cos \theta \mathbf{i} - r \sin \theta \mathbf{j} + r \mathbf{k}.$$

It is already pointing upwards, so we do not need to adjust the sign. Then we have

$$\nabla \times \mathbf{F} = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \partial_x & \partial_y & \partial_z \\ x^2 - y & 4z & x^2 \end{vmatrix} = -4\mathbf{i} - 2x\mathbf{j} + \mathbf{k}.$$

Finally, we have

$$\iint_S (\nabla \times \mathbf{F}) \cdot \mathbf{n} d\sigma = \int_0^{2\pi} \int_0^2 (-4\mathbf{i} - 2r \cos(\theta)\mathbf{j} + \mathbf{k}) \cdot (-r \cos \theta \mathbf{i} - r \sin \theta \mathbf{j} + r \mathbf{k}) dr d\theta = 4\pi.$$